Shock Absorbers - Oil Type

Overview

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For this system, oil is mainly utilized. Compared with other cushioning materials (rubber, spring, air etc.), they are compact and capable of repeatedly absorbing large impact energy softly without rebound. Internal structure and basic principle of oil type shock absorbers are shown as follows.

When an object collides with a piston rod, the oil in the pressure chamber is compressed by a piston.

The clearance between inner tube and piston is so small that compressed oil is forced out

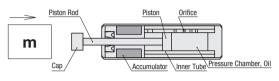
of the orifices. At this point, the impact energy is converted into heat energy by dynamic

The piston rod sinks into the shock absorber body so that the oil equal in volume to the piston moves into the accumulator.

This mechanism provides an ideal shock absorbing action.

Various absorption characteristics can be obtained depending on the number and size of orifices. (Refer to classification according to absorption characteristics

Please note that when the wrong collision speed is selected, some abnormal reaction may occur during collision or the impact energy may not be absorbed in an ideal manner



Procedure of Selection

(1) Calculation of Inertial Energy (E₁)

According to examples of calculation for selection, calculate inertial energy based on collision mass (m), collision velocity (V), moment of inertia (I) and collision angular velocity (ω).

2) Temporary Decision of Absorber Stroke

Obtain the temporary stroke (S') based on Fig. 1.

3 Calculation of Additional Energy (E2')

Confirm whether there is propulsion (F) or not and calculate the additional energy according to examples of calculation for selection.

(4) Calculation of Total Energy

Calculate the total energy from the sum of inertial energy (E1) and additional energy (E2').

5 Check Equivalent Mass

According to examples of calculation for selection, calculate the equivalent mass and confirm whether it is less than the max. equivalent mass in the catalog (me').

6 Select Absorption Characteristics Structures from Energy Ratio.

Select an orifice type from Fig. 2 temporarily.

7 Check Max. Absorbed Energy per Minute

Calculate the energy (E_T) corresponding to one minute from the operating cycle (time / min) and total energy, and confirm whether or not the value is within the operating range.



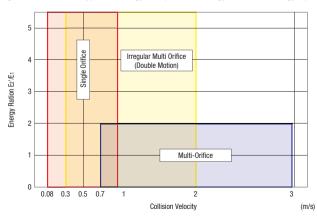
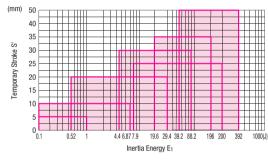


Fig. 1 Calculate the temporary stroke S' with the Inertial Energy E1. (Adjustable / Fixed Force Type)



- For Single, Irregular Multi, Multi Orifice Types, these are the values of Adjustable / Fixed Types.
- *If both Single Orifice and Multi-Orifice are applicable, select irregular Multi-Orifice.
- *If both Irregular Multi-Orifice and Multi-Orifice are applicable, select
- *For Speed S Type, the collision velocity is $0.08\sim0.5$ m/s.

| Exam | ples of Calculation for Selection | Ex.) Pure Inertial Collision (Horizontal Collision without Thrust Force) | Ex.) Horizontal Collision with Air Cylinder Thrust Force | Ex.) Soft Stop in the Cylinder Falling | |
|----------------------|-----------------------------------|--|---|--|--|
| С | Example and ollision Conditions | V S <collision conditions=""> m=25kg V=0.6m/s F=0N N=30 times/min</collision> | Air Cylinder S | Collision Conditions> m=15kg V=0.2m/s N=10 times/min Air Cylinder I.D. Ø40 Operating Pressure 0.5MPa | |
| C | ollision Velocity V[m/s] | V=0.6m/s | V=0.6m/s | V=0.2m/s *Collision velocity V is actual measurements or 1.5~2 times the average speed. | |
| Energy | Inertial Energy [J] | E ₁ = $\frac{\text{mxV}^2}{2} = \frac{25\text{x}0.6^2}{2} = 4.5\text{J}$ | $E_1 = \frac{mxV^2}{2} = \frac{30x0.6^2}{2} = 5.4J$ | $E_{1} = \frac{mxV^{2}}{2} = \frac{15x0.2^{2}}{2} = 0.3J$ | |
| ෂ | Temporary Stroke S'Immi | From Fig. 1, S'=20mm (Select Adjustable Type) | From Fig. 1, S'=15mm (Select Adjustable Type) | From Fig. 1, S'=10mm (Select Adjustable Type) | |
| Absorbed | Additional Energy [J] | E2'=0J | Thrust of the cylinder is F=628.4N E2'=FxS'=628.4x0.015=9.4J | Thrust of the cylinder is F=245.4N E2'=(F+mg)xS'=(245.4+15x9.8)x0.01=3.92J | |
| ₽ | Total Energy E'[J] | E'=E1+E2'=4.5+0=4.5J | E'=E1+E2'=5.4+9.4=14.8J | E'=E1+E2'=0.3+3.92=4.22J | |
| Equivalent Mass [kg] | | $me' = \frac{2xE'}{V^2} = \frac{2x4.5}{0.6^2} = 25kg$ | $=\frac{2xE'}{V^2} = \frac{2x14.8}{0.6^2} = 82.2kg$ $me' = \frac{2xE'}{V^2} = \frac{2x4.22}{0.2^2} = 211kg$ | | |
| Te | emporary Selection | Select Adjustable Type Select L from the collision velocity. Select MAC1612 from E and me'. (Stroke S=12mm) | Select Adjustable Type Select medium speed M from the collision velocity. Select MAC2016M from E' and me'. Stroke S=16mm | Select Adjustable Type Select ultra low speed S from Fig. 2. Stroke Select MAC1612S from E' and me'. S=12mm | |
| Recalculation - | | $E_{2}=0J$ $me=\frac{2xE}{V^2}=25kg$ | $E_2=FxS=10.1J$ $me=\frac{2xE}{V^2}=86.1kg$ | $me = \frac{2\lambda C}{86.1 \text{kg}} = 86.1 \text{kg}$ $me = \frac{2\lambda C}{86.1 \text{kg}} = 250 \text{kg}$ | |
| Energy per Minute ET | | ET=ExN=4.5x30=135J/min | ET=ExN=15.5Jx20=310J/min | ET=ExN=5.01x10=50.1J/min | |
| | Confirmation | E, me, N and Eτ are OK. Select MAC1612L | E, me, N and ET are OK. Select MAC2016M | E, me, N and ET are OK. Select MAC1612S | |

*For horizontal collision without thrust force, select the Orifice Type only by collision velocity.

| Ex.) Horizontal Collision with Belt Conve | | Ex.) Horizontal Collision with Belt Conveyor Thrust Force | Ex.) Collision with Synchronous Motor Driven Load | Ex.) Horizontal Rotary Collision with Torque | |
|---|---------------------------------|---|--|---|--|
| C | Example and ollision Conditions | $\begin{array}{c} V \\ \mu \\ \hline \end{array} \\ \begin{array}{c} S \\ \hline \\ W=0.5 \\ N=10 \\ \end{array} \\ \begin{array}{c} Collision Conditions \\ m=5kg \\ V=0.5m/s \\ N=10 \\ times/min \\ \end{array}$ | Collision Conditions> | Collision Conditions> =125.5kg·m² ω=1.8rad/s R=1.25m N=6 times/min T=68.6N·m | |
| Commence to conty time of | | | V=Rω=0.4x5.6=2.24m/s | V=Rω=1.25x1.8=2.25m/s | |
| Energy | Inertial Energy[J] | $E_1 = \frac{mxV^2}{2} = \frac{5x0.5^2}{2} = 0.625J$ | $E_{1} = \frac{I\omega^{2}}{2} = \frac{0.12x5.6^{2}}{2} = 1.88J$ | $E_1 = \frac{I\omega^2}{2} = \frac{125.5 \times 1.8^2}{2} = 203.31 \text{J}$ | |
| E E | Temporary Stroke Summit | From Fig. 1, S'=5mm (Select Fixed Force Type) | From Fig. 1, S'=10mm (Select Adjustable Type) | From Fig. 1, S'=50mm (Select Adjustable Type) | |
| sorbed | Additional Energy [J] | F=µmg=0.4x5x9.8=19.6N E2'=F·S'=19.6x0.005=0.098J | E2'=(F+mg)xS'=(59.3+1x9.8)x0.01=0.69J | $E_2' = \frac{T}{R} \cdot S' = \frac{68.6}{1.25} \times 0.05 = 2.74J$ | |
| Ab | Total Energy E'[J] | E'=E1+E2'=0.625+0.098=0.723J | E'=E1+E2'=1.88+0.69=2.57J | E'=E1+E2'=203.31+2.74=206.05J | |
| Equivalent Mass [kg] $me' = \frac{2xE'}{V^2} = \frac{2x0.723}{0.5^2} = 5.8kg$ | | $me' = \frac{2xE'}{V^2} = \frac{2x0.723}{0.5^2} = 5.8kg$ | $me' = \frac{2xE'}{V^2} = \frac{2x2.57}{2.24^2} = 1.0kg$ $me' = \frac{2xE'}{V^2} = \frac{2x206.05}{2.25^2} = 81.4kg$ | | |
| Temporary Selection | | Select Fixed Force Type Select Single Orifice from V Select MAKC1005B from E' and me'. S=5mm | Select Adjustable Type Select Multi-Orifice from Fig. 2. Select MAC1210H from E' and me'. (Stroke S=10mm) | Select Adjustable Type Select Speed H Type from Fig. 2. (Stroke Select MAC3650H from E' and me'. (S=50mm) | |
| Recalculation | | $E_2=E_2'=0.098J$ $E_2=E_1+E_2=0.723J$ $me=\frac{2xE}{V^2}=5.8kg$ | E2=0.69J E=E1+E2=2.57J me=1.0kg | $E_2 = \frac{T}{R} \cdot S = 2.74J$ $me = \frac{2xE}{V^2} = 81.4kg$ $E = E_1 + E_2 = 206.05J$ | |
| E | nergy per Minute ET | E _T =ExN=0.723x20=14.46J/min | E _T =ExN=2.57x10=25.7J/min | E _T =ExN=206.05x6=1236.3J/min | |
| | Confirmation | E, me, N and Eτ are 0K. Select MAKC1005B | E, me, N and ET are OK. Select MAC1210H | E, me, N and ET are OK. Select MAC3650H | |

| Shock Absorbers (P355~360) Classification according to absorption characteristics structures | | | | | | | |
|--|--------------------------------------|--|--|---|--|--|--|
| Structure Adjustable* Fixed Force Type | | | | | | | |
| Single Orifice | S Type A Type B Type L Type | | Single orifice structure has the same resistance properties as forms of a dashed pot structure with a space between the piston and cylinder tube, a single tube structure with an orifice in the piston, and a double tube single orifice structure. Ex. Description of a Single Tube Structure A piston with a single orifice slides into an oil-filled cylinder tube. Because the office area is constant over the entire stroke, as the shock absorption characteristics shown in the right graph, the resistance is the largest immediately after a collision but gradually reduces speed as the stroke continues. | F | | | |
| Irregular Multi Orifice | Medium Speed M Type | | In this double-tube structure, the piston slides in the inner tube. This inner tube has several orifices along the direction of strokes, and not only constant energy but energy depending on various purposes can be absorbed. It is designed to absorb kinetic energy during the first half of stroke and control speed during the second half. Therefore, it is well suited to absorb energy against air cylinder thrust. | F | | | |
| Multi Orifice | High Speed H Type | | In this double-tube structure, the piston slides in the inner tube. This inner tube has several orifices along the direction of strokes. Because the orifice area becomes smaller gradually as the stroke speed slows down, drag remains largely constant, though the drag fluctuates like a ripple. | F | | | |

^{**}P*Adjustable Type No. 0806M is single orifice structure and No. 3625L Type is multi-orifice structure.

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