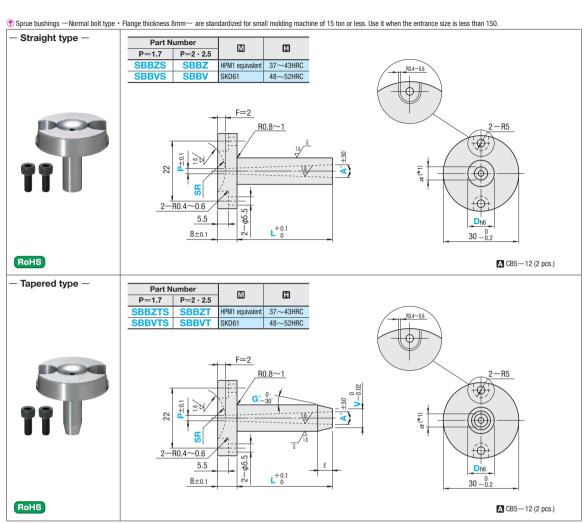
Non JIS material definition is listed on P.1351 - 1352

Quotation

Spec.



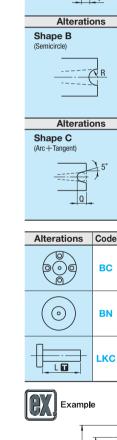
	Dh6		Part Numb	er		L(*2)	SR	Р	A°	V	G°
	Dno	Туре			D	0.1mm increments	on .	F	0.5° increments	0.1mm increments	1° increments
10	0 -0.009	—Straight type— (HPM1 equivalent) (SKD61) —Tapered type— (HPM1 equivalent) (SKD61)	When P=1.7 (SBBZS SBBVS SBBZTS SBBVTS	SBBZ SBBV SBBZT SBBVT	10	0~80.0	11	1.7 ^(*4) 2 2.5	(*3) 1~4	$D>V \ge \alpha + 2$ Available for tapered type only	1∼10 Available for tapered type only
(*1) The value of α is set in accordance with L dimension. (*2) L dimension is restricted by A. (*3) L dimension limits A Lmax. 1 50 (*4) P=1.7 is applicable for A° 1, 2 only until L=40. (*5) L dimension limits • Straight type • Tapered type • Tapered type • Tapered type • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv. • $\alpha \ge 2$ (Calculation of α value) $\alpha = P + 2(L + 6)\tan\frac{A}{2}$ Conv.							When us When FC When FC	nversion Chart of Trigonometric Functions Σ P.1337 When using FC code When FC1 α = P+2(L+7)tan $\frac{A}{2}$ When FC3 α = P+2(L+5)tan $\frac{A}{2}$ s to be L- ℓ \geq 10.			

Α

Р

SR -

SBBV 10 - 50.0 - SR11 - P2 - A2 SBBVT10 - 50.0 - SR11 - P2 - A2



2-R0.4~0.6

Quotation

Alterations

Shape A (Trapezoid) R0.5 R1.5	The tr	AJW, ALW an	per angle, w	working lim hich was pre	eviously fixe	0.6)≧W d at 10°, is		able from 10°°. ". If you do	Designation method AIW4—GC7 +Bolt hole position KC position (When KC code is used) and 7°. not make a specification, (AHW4)	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ction
Alterations	Code	BIR	BHR	BXR	BTR	BJR	BLR	BPR	Sp	ec.	
Shape B (Semicircle)	Spec.		10	10	10	1\$	10	10	Designation method BXR2 +Bolt hole position KC position	• R dimension sel 1 1.25 1.5	ection
R	1Code	1Code [1			(When KC code is used)1.51.7		
	♠ BTR,	$\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $									
Alterations	Code	CIQ	CHQ	CXQ	CTQ	CJQ	CLQ	CPQ	Sp	ec.	
Shape C (Arc+Tangent)	Spec.		100						Designation method CTQ3 +Bolt hole position KC position	• Q dimension seli 2 2.5 3	ection
===	1Code			Quotation				(When KC code is used)3			
Q	◆ CTQ,	\P CTQ, CJQ, CLQ and CPQ have working limits (α -0.6) \geqq 0×1.09									
									1	1.0	
Alterations Code	Spec.				1Code	Α	teration	s Code	e Spec. 1Code		

L - SR - P - A - V - G - (AIW · AXW···etc.)

Code AIW AHW AXW ATW AJW ALW APW

Increases No. of holt holes

Decreases No. of bolt holes.

• Available for equivalent of material HPM1

\<u>co</u>

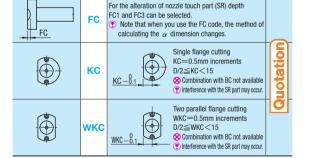
No. of bolt holes : 2 ··· 0

L dimension tolerance alteration

L + 0.1 L _ 0.02

① L dimension can be designated at 0.01mm increments when LKC is used.

No. of bolt holes: 2 · · · 4



[Example of hole machining and assembling for sprue

The position of sprue bushing hole and that of tap hole is adjacent. Please be careful when hole processing because the thickness of X dimension is thin.

■Recommended X Dimension

D	Xmm
8	4.4~4.475
10	3.4~3.475

To decrease the concentration of stress, R part is designed on the root of flange.





L

Part Number -

765 766